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(54) EXHAUST GAS RECIRCULATION IN A TWO STROKE ENGINE

ABGASRÜCKFÜHRSYSTEM IN EINER ZWEITAKTBRENNKRAFTMASCHINE

REMISE EN CIRCULATION DES GAZ D'ÉCHAPPEMENT DE MOTEURS À COMBUSTION À DEUX TEMPS

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(56) References cited:
WO-A-79/00757 **WO-A-94/28299**
DE-A- 2 946 483 **DE-C- 840 479**
GB-A- 2 270 115 **US-A- 3 581 719**
US-A- 4 213 431 **US-A- 4 318 373**

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Description

[0001] This invention relates to internal combustion engines operating on the two stroke cycle and to the management of the combustion process thereof to control the level of contaminants in the exhaust emissions.

[0002] It has in the past been recognised that two stroke cycle engines exhibit poor performance in the area of fuel consumption and also in the area of the level of harmful emissions in the engine exhaust. However, there are substantial benefits to be obtained by wider use of engines operating on the two stroke cycle. Firstly, because of their relatively simple construction, and secondly, because of their relatively small physical size and resultant high power to weight ratio. There has accordingly been considerable development in recent years directed to the control of the combustion process of two stroke cycle engines in a manner to reduce the level of emissions in the exhaust, and/or reduce the fuel consumption.

[0003] It has been recognised that the introduction of exhaust gas into the fuel/air mixture prior to the ignition thereof can contribute to a reduction in the production of NO_x (oxides of nitrogen) during the combustion process, as the presence of exhaust gas in the fuel/air mixture reduces the resultant temperature and pressure in the engine cylinder resulting from the combustion, which is contrary to the high temperature and pressure conditions that promote the creation of NO_x . This process of mixing exhaust gas with the fuel/air mixture is commonly referred to as exhaust gas recirculation (EGR) and is typically achieved by bleeding a controlled quantity of exhaust gas from the exhaust system into the air induction manifold of the engine.

[0004] Although this procedure has been used successfully in four stroke cycle engines, it is not as effective when applied to two stroke cycle engines, due principally to the low level of vacuum existing downstream from the conventional throttle in the air induction system. Hence, this would result in a low rate of intake of exhaust gas and in the case of a multi cylinder engine, a poor distribution of the exhaust gas in the induced air. Further, particularly in the case of crankcase scavenged engine, there is a significant time lag in the response by the engine to the introduction of the exhaust gas to the induction system due to the distance it is required to travel before entering the combustion chamber. Also, where exhaust gas is introduced into the induction system of a crankcase scavenged two stroke cycle engine as the air capacity of the crankcase is greater than that of the cylinder, there is a further time lag in a change of rate of exhaust gas supply to the crankcase being seen in the engine cylinder. Also, the particulate materials normally present in exhaust gas can build up on mechanisms in the induction system of such two stroke cycle engines such as throttle valves and crankcase reed valves, and hence interfere in the effective operation thereof.

[0005] It has been previously proposed in publications such as International Patent Publication WO 79/00757 by J.P. Soubis and United States Patent No. 3581719 by Gau to recycle exhaust gas into the combustion chamber for the purpose of returning thereto any unburnt fuel that may be in the exhaust gas. It has long been recognised that carburetted two stroke cycle engines exhibit the problem that part of the air and fuel charge that enters the combustion chamber passes out through the exhaust port prior to the commencement of combustion. The above referred to prior patents each are directed to overcoming this problem by re-directing the fuel rich portion of the exhaust gas back into the air intake or crankcase for recycling into the combustion chamber. As the recycled portion of the exhaust gas is primarily fuel and fresh air, it will not have a significant effect in the control of the generation of NO_x , the problem the present invention is directed to overcoming.

[0006] It is proposed in United States Patent No. 4213431 by Onishi to recycle exhaust gas into the air induction system of a two stroke cycle engine with the intent of control of the generation of NO_x during the combustion process. In this proposal the exhaust gas is introduced directly into the air induction passage upstream of the carburettor. A valve is provided in the duct conveying the exhaust gas to the induction passage, the valve being temperature activated.

[0007] It is the aim of the present invention to provide a method and apparatus for introducing exhaust gas into the combustion chamber of a two stroke cycle engine whereby effective control of the amount and distribution of the exhaust gas can provide the most beneficial results in the management of exhaust emissions.

[0008] With this aim in view, there is provided a method of operating a two stroke cycle crankcase scavenged internal combustion engine characterised by selectively delivering exhaust gas from a location downstream of the engine exhaust port to the engine crankcase to be delivered from the crankcase to a combustion chamber of the engine, controlling the quantity of exhaust gas delivered to the crankcase during each cycle of the engine in accordance with the engine operating conditions for NO_x reduction, and timing the delivery of the exhaust gas to the crankcase with respect to the cycle of the engine.

[0009] As the admission of the exhaust gas to the crankcase is principally for the control of exhaust emissions, it is not necessary, and in some circumstances can be undesirable, to admit exhaust gas to the crankcase under all operating conditions. Accordingly, it is desirable to be selective in the introduction of the exhaust gas to the crankcase and also to control the rate of supply of exhaust gas. This control of the exhaust gas supply to the engine crankcase can be achieved by an ECU managed control valve provided between the exhaust system of the engine and the engine crankcase to control the exhaust gas flow to the crankcase. The ECU managing the control valve preferably receives inputs

regarding engine operating conditions and in particular, engine load, speed and temperature conditions. The ECU determines from these inputs when exhaust gas is required to be introduced to the crankcase and the quantity thereof required.

[0010] Preferably the control valve incorporates a position feedback means to indicate to the ECU the actual position of the valve to thereby permit comparison of the actual position with the required position, thereby enhancing the accuracy of the control of the rate of supply of exhaust gas to the crankcase. Alternatively, the ECU can be programmed to determine the actual mass of exhaust gas delivered to the crankcase each cycle and to compare that mass with the required mass of exhaust gas for the existing engine operating conditions. Any correction required can then be effected by adjustment of the rate of supply of exhaust gas to the crankcase via the ECU controlled valve.

[0011] In a multi-cylinder two stroke cycle crankcase scavenged engine, where each cylinder has an individual crankcase compartment, a plenum chamber may be provided which communicates individually with the crankcase of each cylinder, with exhaust gas from one or more of the engine cylinders being provided to the plenum chamber. Under normal conditions, it may only be necessary to supply exhaust gas from one or some of the cylinders to the plenum chamber, even where a greater number of cylinders are supplied with exhaust gas from the plenum chamber.

[0012] In part, the exhaust gas performs the emission control function by reducing the overall cycle temperature and pressure in the engine cylinder during combustion, as the exhaust gas has a higher specific heat than air and hence will reduce the overall cycle temperature of the gases in the combustion chamber. As high temperature is one of the requirements for the production of NO_x , this reduction in overall cycle temperature contributes to a reduction in the production of NO_x . It is also to be noted that the exhaust gas of a two stroke cycle engine has a higher oxygen content than that of a four stroke cycle engine and therefore more exhaust gas is required to be recycled in a two stroke engine to receive a comparable level of NO_x control.

[0013] The use of a plenum chamber in a multi-cylinder engine can readily be made to contribute to a reduction in the temperature of the exhaust gas delivered to the combustion chamber and in addition, provision can be made to enhance the dissipation of heat from the plenum chamber to achieve a further temperature reduction. Also a heat exchanger can be incorporated in the path of the exhaust gas to the engine crankcase to further contribute to a reduction of the temperature of the exhaust gas prior to admission to the crankcase. Conveniently, the duct conveying the exhaust gas to the cylinder or cylinders or to the plenum chamber can be cooled by external fins or by liquid or water cooling such as from the engine cooling system.

[0014] In accordance with another aspect of the in-

vention, there is provided a method as claimed in any one of claims 1 to 7 including cooling the exhaust gas prior to delivery to the crankcase.

[0015] In one embodiment, a piston controlled port can be provided in the lower portion of the engine cylinder wall to communicate with the crankcase of that particular cylinder and also with the supply of exhaust gas, such as via the plenum chamber. Preferably, the port communicates with the exhaust system via an ECU controlled valve as previously described. The port is located so that it will be exposed whilst the piston is within a limited extent of movement on either side of the top dead centre position thereof which represents the period of minimum pressure (subatmospheric) in the crankcase. Conveniently, the port can be located so as to be open for approximately 40° to 60° of crankshaft rotation to each side of the top dead centre position of the piston stroke.

[0016] It may be convenient in some engine configurations to provide two or more such piston controlled ports for each crankcase to provide a relatively large flow area for the exhaust gas into the crankcase. Preferably, the port or ports have the major dimension thereof in the circumferential direction of the cylinder to provide the maximum open port area during the restricted port open period. It has been found that the use of a piston controlled port to control the timing of admission of the exhaust gas results in improved equitable cylinder to cylinder distribution of the exhaust gas.

[0017] Preferably, the ECU managing the degree of opening of the valve is programmed to control the valve by reference to a speed/load based look-up map. The load may be plotted on a FPC (fuel per cycle) basis. In addition, the ECU preferably also responds to engine temperature since, for example, at some cold start conditions, the addition of exhaust gas can be detrimental to the engine operating stability.

[0018] In an engine where catalyst unit is provided in the exhaust system the exhaust gas can be taken from the exhaust system either upstream or downstream of the catalyst unit, but preferably the exhaust gas is recirculated from downstream of the catalyst unit.

[0019] The invention also provides a crankcase scavenged two stroke cycle engine characterised by means to selectively convey exhaust gas from an engine exhaust system to at least one crankcase of the engine, means to regulate the mass of exhaust gas delivered to said crankcase each engine cycle for NO_x reduction, and means for controlling the timing of the delivery of said exhaust gas to the crankcase in relation to the engine cycle.

[0020] The invention will be more fully understood from the following description of two alternative arrangements of crankcase scavenged two stroke cycle engines.

[0021] In the drawings:

Figure 1 is a transverse sectional view of a crank-

case scavenged two stroke cycle engine incorporating one embodiment of an exhaust gas recirculation system; and

Figure 2 is a longitudinal sectional plan view of a portion of a three cylinder engine incorporating the exhaust gas recirculation system as shown in Figure 1.

[0022] Referring now to Figure 1 of the drawings, there is shown a partial transverse section of a crankcase scavenged two stroke cycle engine wherein the cylinder block is in cross section and the cylinder head and injector equipment are in full outline. For the purposes of clarity, the piston and connecting rod are not shown. The engine is basically of conventional construction having a cylinder 30 in which a piston (not shown) reciprocates and is connected by a connecting rod (not shown) to a crankshaft shown diagrammatically at 31. The cylinder 30 has an exhaust port 32 and a plurality of transfer ports, two of which are shown at 33 and 34 to provide communication between a crankcase 35 and the cylinder 30, subject to the position of the piston within the cylinder 30 as per the conventional two stroke cycle principle. Figure 1 may be of a single cylinder engine or in-line multi-cylinder engine as shown in Figure 2.

[0023] The exhaust port 32 communicates with an exhaust passage 36 which in turn communicates with an exhaust pipe 37 in the mouth of which are located conventional exhaust catalyst elements 38. Downstream of the catalyst elements 38, the exhaust pipe 37 communicates with a branch passage 39 which leads to a cavity 40 in the cylinder block. In Figure 1, the branch passage 39 communicates with the exhaust pipe 37 downstream of the exhaust catalyst elements 38. However, it may alternatively communicate with the exhaust pipe 37 upstream of the catalyst elements 38 where the pressure of the exhaust gas is higher, the temperature is lower, and the oxygen content is lower.

[0024] Communication between the passage 39 and the cavity 40 is under the control of the valve 41 being part of a solenoid valve mechanism 42. The cavity 40 communicates with an internal plenum chamber 43 provided in the cylinder block which, in a multi cylinder engine as shown in Figure 2, communicates individually with each cylinder of the engine through a respective exhaust gas recirculation port 45. The ports 45 are positioned in the wall of the respective cylinders 30 so that during a selected portion of each cylinder cycle, the respective ports 45 are uncovered by the pistons to permit exhaust gas to flow from the plenum chamber 43 into the respective crankcase 35 of each cylinder 30 of the engine.

[0025] As previously indicated, the preferred timing of the opening and closing of the port 45 is within 40° to 60° before and after the top dead centre position of the piston in the respective cylinder 30 and preferably between 45° and 55°. The timing of the supply of exhaust

gas to the crankcase is preferably at a period in the engine cycle when the pressure in the crankcase is below that in the exhaust system. It will be appreciated that the communication between the crankcase 35 and the EGR port 45 is determined by the location of an appropriate aperture in the crankcase wall with respect to the path of the lower edge of the skirt of the piston as is common technology in relation to the control of the flow of gases through the transfer ports of two stroke cycle engines, such as the transfer ports 33 and 34 as shown in Figure 1. Further, it is preferred that the port 45 is located on the side of the cylinder against which the piston is thrust so as to effectively seal the port 45 when required.

[0026] As referred to previously, it is desirable to control the delivery of exhaust gas through the port 45 in accordance with variations in engine operating conditions and for this purpose, the solenoid mechanism 42, or other suitable mechanism that controls the operation of the valve 41 is under the control of a programmed ECU 46 incorporating appropriate look-up maps. Usually, the map is arranged so that the valve 41 controlling the exhaust gas flow to the crankcase 35 is ramped rapidly from closed to open once the fuelling rate increases above a selected level. The solenoid mechanism 42 is typically provided with a valve element position sensor 47 which provides feedback information to the ECU 46 to facilitate the accurate control of the position of the valve 41 to achieve the required rate of supply of exhaust gas to the respective crankcase cavities 35 of the engine. The ECU 46 typically receives inputs indicating the engine speed, engine load, and engine temperature. Provision can also be made for the ECU to monitor and adjust the movement of the valve 41 to detect and correct for the effects of carbon build-up on the valve of seat in which it operates.

[0027] As an alternative to the use of look-up maps to control the rate of supply of exhaust gas, the ECU can be programmed to determine the mass of air entering each crankcase 35 and to determine the combined exhaust gas and air mass in the respective crankcase 35 at a selected point in the cycle of that engine cylinder 30. The mass of air entering the crankcase 35 can be determined by a conventional hot wire air flow meter in the air induction passage, and the mass of air and exhaust gas can be determined by measuring the temperature and pressure in the crankcase 35 at a preset point in the engine cycle when the volume of the space in the crankcase 35 is known. From these two mass determinations, the actual mass of exhaust gas can be determined and compared with the required amount of exhaust gas, thus determining if adjustment is required to be made to the rate of supply of the exhaust gas. This method of determining the exhaust gas content within the crankcase can be used in conjunction with other forms of control of EGR than that described herein. Also, by determining the air mass in the crankcase when no exhaust gas is present therein, the accuracy of the measurement process can be checked by comparing

the calculated air mass with the air mass as determined by the hot wire air flow meter.

[0028] Other engine operating parameters that can be controlled, in conjunction with the supply of exhaust gas to the crankcase 35, include advance of the ignition spark to increase combustion temperature, and use of a back pressure valve in the exhaust system, downstream of the point of exhaust gas take-off to control the rate of exhaust gas available for supply to the combustion chamber. The greater the back pressure in the exhaust system, the greater the pressure and hence the rate of supply of exhaust gas for admission to the crankcase 35.

[0029] Also, the exhaust gas to be delivered to the engine cylinder 30 can be passed through a heat exchanger or otherwise cooled means prior to entry to the crankcase 35 in order to increase the density thereof whereby a greater mass of exhaust gas would then be available for delivery to the crankcase 35. In Figure 1, the branch passage 39 communicates with the exhaust pipe 37 downstream of the catalyst element 38. However, it may alternatively communicate with the exhaust pipe 37 upstream of the catalyst element where the pressure of the exhaust gas is higher and the temperature lower.

[0030] In practice, it has been found convenient to provide multiple delivery locations for the exhaust gas to the plenum chamber to assist in achieving substantial uniform distribution of the exhaust gas from a common plenum chamber into the respective crankcase of each cylinder.

[0031] Also, in the higher range of operating speeds, the rate of rise of the crankcase pressure, after top dead centre position of the piston, is such that a reverse flow of air from each respective crankcase through the ports 45 can occur. This can lead to a dilution of the exhaust gas in the plenum chamber and possibility of unequal distribution of exhaust gas to the respective engine cylinders. This problem can be at least reduced by suitable selection of the length of the ports 45 between the plenum chamber 43 and the crankcase chambers 35, so that any reverse flow of gas from the crankcase is substantially retained with the port 45 associated with that crankcase chamber 35 and not passed into the plenum chamber 43.

Claims

1. A method of operating a two stroke cycle crankcase scavenged internal combustion engine characterised by selectively delivering exhaust gas from a location downstream of the engine exhaust port (32) to the engine crankcase (35) to be delivered from the crankcase (35) to a combustion chamber (30) of the engine, controlling the quantity of said exhaust gas delivered to the crankcase (35) during each cycle of the engine in accordance with engine operating conditions for NO_x reduction, and timing
2. A method as claimed in claim 1 wherein the delivery of the exhaust gas to the crankcase (35) is commenced after the closing of transfer ports (33) that communicate the crankcase (35) with the combustion chamber (30).
3. A method as claimed in claim 1 or 2 wherein the timing of the delivery of the exhaust gas to the crankcase (35) is controlled by the location of the port (45) in the crankcase (35) that is opened and closed in response to movement of a piston in a cylinder.
4. A method as claimed in claim 1, 2 or 3, wherein the delivery of the exhaust gas to the crankcase (35), commences between 60 and 40 degrees before the top dead centre point in the combustion chamber cycle.
5. A method as claimed in claim 1, 2 or 3, wherein the delivery of the exhaust gas to the crankcase (35) commences between 55 and 45 degrees before the top dead centre point in the combustion chamber cycle.
6. A method as claimed in any one of claims 1 to 5, wherein the control of the quantity of exhaust gas delivered to the crankcase is determined with reference to engine load and/or speed.
7. A method as claimed in claim 6 wherein the control of the quantity of exhaust gas delivered to the crankcase is also determined with reference to engine temperature.
8. A method as claimed in any one of claims 1 to 7 including cooling the exhaust gas prior to delivery to the crankcase.
9. A method as claimed in any one of claims 1 to 8 wherein a catalytic treatment means is located downstream of the engine exhaust port and wherein the exhaust gas is recirculated from downstream of a catalytic treatment means.
10. A method as claimed in any one of the preceding claims wherein the selectively delivered exhaust gas principally consists of combusted by-products from a previous engine cycle.
11. A crankcase scavenged two stroke cycle engine characterised by means to selectively convey exhaust gas from an engine exhaust system (37) to at least one crankcase (35) of the engine, means to regulate the mass of exhaust gas delivered to said

the exhaust gas delivery to the crankcase (35) with respect to the engine cycle.

crankcase (35) each engine cycle for NO_x reduction, and means for controlling the timing of the delivery of said exhaust gas to the crankcase (35) in relation to the engine cycle.

12. The engine claimed in claim 11 wherein said means for controlling the timing of delivery is a port (45) in the crankcase wall which is cyclically opened and closed in response to reciprocation of a piston in a cylinder arranged to receive an air charge from said crankcase (35).
13. The engine claimed in claim 12 wherein the said piston and port (45) are relatively arranged to commence opening of the port at between 60 and 40 degrees before the top dead centre position of the piston in said cylinder.
14. The engine claimed in claim 11, 12 or 13 wherein the means to regulate the mass of exhaust gas includes valve means (41) selectively operable to control exhaust gas flow along said means to convey the exhaust gas.
15. The engine claimed in claim 14 wherein the valve means (41) is operable when open to permit said exhaust gas flow to also regulate the rate of flow of the exhaust gas.
16. The engine claimed in claim 15 wherein said means to regulate the mass of gas flow includes feedback means to determine the actual mass of exhaust case delivered to the crankcase (35) per cycle and means to correct variations between the required quantity and delivered quantity of exhaust gas delivered to the crankcase (35) per cycle.
17. The engine claimed in any one of claims 11 to 16 wherein the engine exhaust system includes a catalytic treatment means, the exhaust gas being recirculated from downstream of the catalytic treatment means.
18. The engine claimed in any one of claims 11 to 17 wherein the selectively conveyed exhaust gas principally consists of combusted by-products from a previous engine cycle.

Patentansprüche

1. Verfahren zum Betreiben eines Zweitaktverbrennungsmotors oder einer Zweitaktverbrennungsmaschine mit Kurbelgehäusespülung, gekennzeichnet durch das selektive Abgeben von Abgas von einer Stelle strömungsabwärts der Motorabgasöffnung (32) zum Motorkurbelgehäuse (35), das vom Kurbelgehäuse (35) zu einer Verbrennungskammer

(30) des Motors abzugeben ist, Steuern der Menge des zum Kurbelgehäuse (35) abgegebenen Abgases während jedes Zyklus des Motors entsprechend den Motorbetriebsbedingungen zur Reduzierung von NO_x, sowie Zeitsteuern der Abgasabgabe zum Kurbelgehäuse (35) bezüglich des Motorzyklus.

2. Verfahren nach Anspruch 1, bei welchem die Abgabe des Abgases zum Kurbelgehäuse (35) nach dem Schließen von Übergangsöffnungen (33) begonnen wird, die das Kurbelgehäuse (35) mit der Verbrennungskammer (30) verbinden.
3. Verfahren nach Anspruch 1 oder 2, bei welchem die Zeitsteuerung der Abgabe des Abgases zum Kurbelgehäuse (35) durch die Anordnung der Öffnung (45) im Kurbelgehäuse (35) gesteuert wird, die in Abhängigkeit von der Bewegung eines Kolbens in einem Zylinder geöffnet und geschlossen wird.
4. Verfahren nach einem der Ansprüche 1, 2 oder 3, bei welchem die Abgabe des Abgases zum Kurbelgehäuse (35) zwischen 60 und 40 Grad vor dem oberen Totpunkt im Verbrennungskammerzyklus beginnt.
5. Verfahren nach einem der Ansprüche 1, 2 oder 3, bei welchem die Abgabe des Abgases zum Kurbelgehäuse (35) zwischen 55 und 45 Grad vor dem oberen Totpunkt im Verbrennungskammerzyklus beginnt.
6. Verfahren nach einem der Ansprüche 1 bis 5, bei welchem die Steuerung der Menge des zum Kurbelgehäuse abgegebenen Gases in Bezug auf die Motorbelastung und/oder Drehzahl bestimmt wird.
7. Verfahren nach Anspruch 6, bei welchem die Steuerung der Menge des zum Kurbelgehäuse abgegebenen Abgases auch bezüglich der Motortemperatur bestimmt wird.
8. Verfahren nach einem der Ansprüche 1 bis 7, bei welchem das Abgas vor der Abgabe an das Kurbelgehäuse gekühlt wird.
9. Verfahren nach einem der Ansprüche 1 bis 8, bei welchem eine Einrichtung zur katalytischen Behandlung strömungsabwärts der Motorabgasöffnung angeordnet wird und bei welchem das Abgas von strömungsabwärts der Einrichtung zur katalytischen Behandlung zirkuliert wird.
10. Verfahren nach einem der vorangehenden Ansprüche, bei welchem das selektiv abgegebene Abgas hauptsächlich aus verbrannten Nebenprodukten aus einem vorangehenden Motorzyklus besteht.

11. Zweitaktverbrennungsmotor oder Zweitaktverbrennungsmaschine mit Kurbelgehäusespülung, gekennzeichnet durch eine Einrichtung zur selektiven Förderung von Abgas aus einem Motorabgassystem (37) zu wenigstens einem Kurbelgehäuse (35) des Motors, eine Einrichtung zum Regulieren der Masse des zum Kurbelgehäuse (35) gelieferten Abgases in jedem Motorzyklus zur Reduzierung von NO_x , und eine Einrichtung zum Steuern des Zeitpunktes der Abgabe des Abgases zum Kurbelgehäuse (35) in Beziehung auf den Motorzyklus. 5
12. Motor nach Anspruch 11, bei welchem die Einrichtung zum Steuern des Zeitpunktes der Abgabe eine Öffnung (45) in der Kurbelgehäusewand ist, die in Abhängigkeit vom Hin- und Hergehen eines Kolbens in einem Zylinder für die Aufnahme einer Luftcharge aus dem Kurbelgehäuse (35) zyklisch geöffnet und geschlossen wird. 10
13. Motor nach Anspruch 12, bei welchem der Kolben und die Öffnung (45) gegenseitig so angeordnet sind, daß das Öffnen der Öffnung zwischen 60 und 40 Grad vor dem oberen Totpunkt des Kolbens im Zylinder beginnt. 15
14. Motor nach einem der Ansprüche 11, 12 oder 13, bei welchem die Einrichtung zum Regeln der Masse des Abgases eine Ventileinrichtung (41) umfaßt, die zur Steuerung der Abgasströmung längs der Einrichtung zum Fördern des Abgases selektiv betätigbar ist. 20
15. Motor nach Anspruch 14, bei welchem die Ventileinrichtung (41), wenn sie geöffnet ist, so betätigbar ist, daß sie Abgasströmung zuläßt, um auch die Strömungsgeschwindigkeit des Abgases zu regeln. 25
16. Motor nach Anspruch 15, bei welchem die Einrichtung zum Regulieren der Masse der Gasströmung eine Rückführungseinrichtung umfaßt, um die tatsächliche Masse des zum Kurbelgehäuse (35) je zyklus abgegebenen Abgases zu bestimmen, sowie eine Einrichtung zum Korrigieren von Änderungen zwischen der erforderlichen Menge und der abgegebenen Menge des zum Kurbelgehäuse (35) je Zyklus abgegebenen Abgases. 30
17. Motor nach einem der Ansprüche 11 bis 16, bei welchem das Motorabgassystem eine katalytische Behandlungseinrichtung enthält, wobei das Abgas von stromabwärts der katalytischen Behandlungseinrichtung rezirkuliert wird. 35
18. Motor nach einem der Ansprüche 11 bis 17, bei welchem das wahlweise geförderte Abgas hauptsächlich aus verbrannten Nebenprodukten aus einem vorherigen Motorzyklus besteht. 40

Revendications

1. Procédé de fonctionnement d'un moteur à combustion interne à deux temps à balayage du carter, caractérisé en ce qu'il fournit de manière sélective au carter (35), depuis un endroit situé en aval de la lumière d'échappement (32) du moteur, le gaz d'échappement qui doit être fourni, depuis le carter (35), à une chambre de combustion (30) du moteur, en ce qu'il commande la quantité dudit gaz d'échappement fourni au carter (35) durant chaque cycle du moteur en fonction des conditions de fonctionnement du moteur pour réaliser la réduction de NO_x , et en ce qu'il régule l'approvisionnement du carter (35) en gaz d'échappement en fonction du cycle du moteur. 5
2. Procédé selon la revendication 1, dans lequel l'approvisionnement du carter (35) en gaz d'échappement commence après la fermeture des lumières de transfert (33) qui établissent une communication entre le carter (35) et la chambre de combustion (30). 10
3. Procédé selon la revendication 1 ou 2, dans lequel la régulation de l'approvisionnement du carter (35) en gaz d'échappement est commandée par l'emplacement de la lumière (45) du carter (35) qui est ouverte et fermée en fonction du mouvement d'un piston dans un cylindre. 15
4. Procédé selon la revendication 1, 2 ou 3, dans lequel l'approvisionnement du carter (35) en gaz d'échappement commence entre 60 et 40 degrés avant le point mort haut dans le cycle de la chambre de combustion. 20
5. Procédé selon la revendication 1, 2 ou 3, dans lequel l'approvisionnement du carter (35) en gaz d'échappement commence entre 55 et 45 degrés avant le point mort haut dans le cycle de la chambre de combustion. 25
6. Procédé selon l'une quelconque des revendications 1 à 5, dans lequel la commande de la quantité de gaz d'échappement fournie au carter est déterminée en fonction de la charge et/ou vitesse du moteur. 30
7. Procédé selon la revendication 6, dans lequel la commande de la quantité de gaz d'échappement fournie au carter (35) est déterminée en fonction de la température du moteur. 35
8. Procédé selon l'une quelconque des revendications 1 à 7, comprenant le refroidissement du gaz d'échappement avant son arrivée au carter. 40

9. Procédé selon l'une quelconque des revendications 1 à 8, dans lequel des moyens de traitement catalytique se trouvent en aval de la lumière d'échappement du moteur et dans lequel le gaz d'échappement est recyclé depuis un endroit situé en aval de moyens de traitement catalytique. 5
10. Procédé selon l'une quelconque des revendications précédentes, dans lequel le gaz d'échappement fourni de manière sélective est principalement constitué de sous-produits, issus d'une combustion d'un cycle de moteur précédent. 10
11. , Moteur à deux temps à balayage du carter, caractérisé par des moyens destinés à acheminer de manière sélective le gaz d'échappement depuis un système d'échappement de moteur (37) vers au moins un carter (35) du moteur, des moyens pour réguler la masse de gaz d'échappement fournie audit carter (35) durant chaque cycle de moteur pour réaliser la réduction de NO_x et des moyens pour commander la régulation de l'approvisionnement dudit carter (35) en ledit gaz d'échappement en fonction du cycle de moteur. 15 20 25
12. Moteur selon la revendication 11, dans lequel ledit moyen pour commander la régulation de l'approvisionnement est une lumière (45) dans la paroi du carter qui est ouverte et fermée de manière cyclique en fonction du mouvement de va-et-vient d'un piston dans un cylindre agencé pour recevoir une charge d'air provenant dudit carter (35). 30
13. Moteur selon la revendication 12, dans lequel lesdits piston et lumière (45) sont agencés de manière relative pour commencer l'ouverture de la lumière à entre 60 et 40 degrés avant la position de point mort haut du piston dans ledit cylindre. 35
14. Moteur selon la revendication 11, 12, ou 13, dans lequel les moyens pour réguler la masse de gaz d'échappement comprennent des moyens formant clapet (41) pouvant être actionnés de manière sélective pour commander l'écoulement de gaz d'échappement le long desdits moyens destinés à acheminer le gaz d'échappement. 40 45
15. Moteur selon la revendication 14, dans lequel les moyens formant clapet (41) peuvent être actionnés lorsqu'ils sont ouverts pour permettre audit écoulement de gaz d'échappement de réguler également le débit d'écoulement du gaz d'échappement. 50
16. Moteur selon la revendication 15, dans lequel lesdits moyens pour réguler la masse d'écoulement de gaz comprennent des moyens de rétroaction destinés à déterminer la masse réelle de gaz d'échappement fournie au carter (35) par cycle et des moyens pour corriger les variations entre la quantité de gaz d'échappement nécessaire et la quantité de gaz d'échappement fournie au carter (35) par cycle. 55
17. Moteur selon l'une quelconque des revendications 11 à 16, dans lequel le système d'échappement du moteur comprend des moyens de traitement catalytique, le gaz d'échappement étant recyclé depuis l'endroit situé en aval des moyens de traitement catalytique.
18. Moteur selon l'une quelconque des revendications 11 à 17, dans lequel le gaz d'échappement acheminé de manière sélective est principalement constitué de sous-produits issus de la combustion d'un cycle de moteur antérieur.

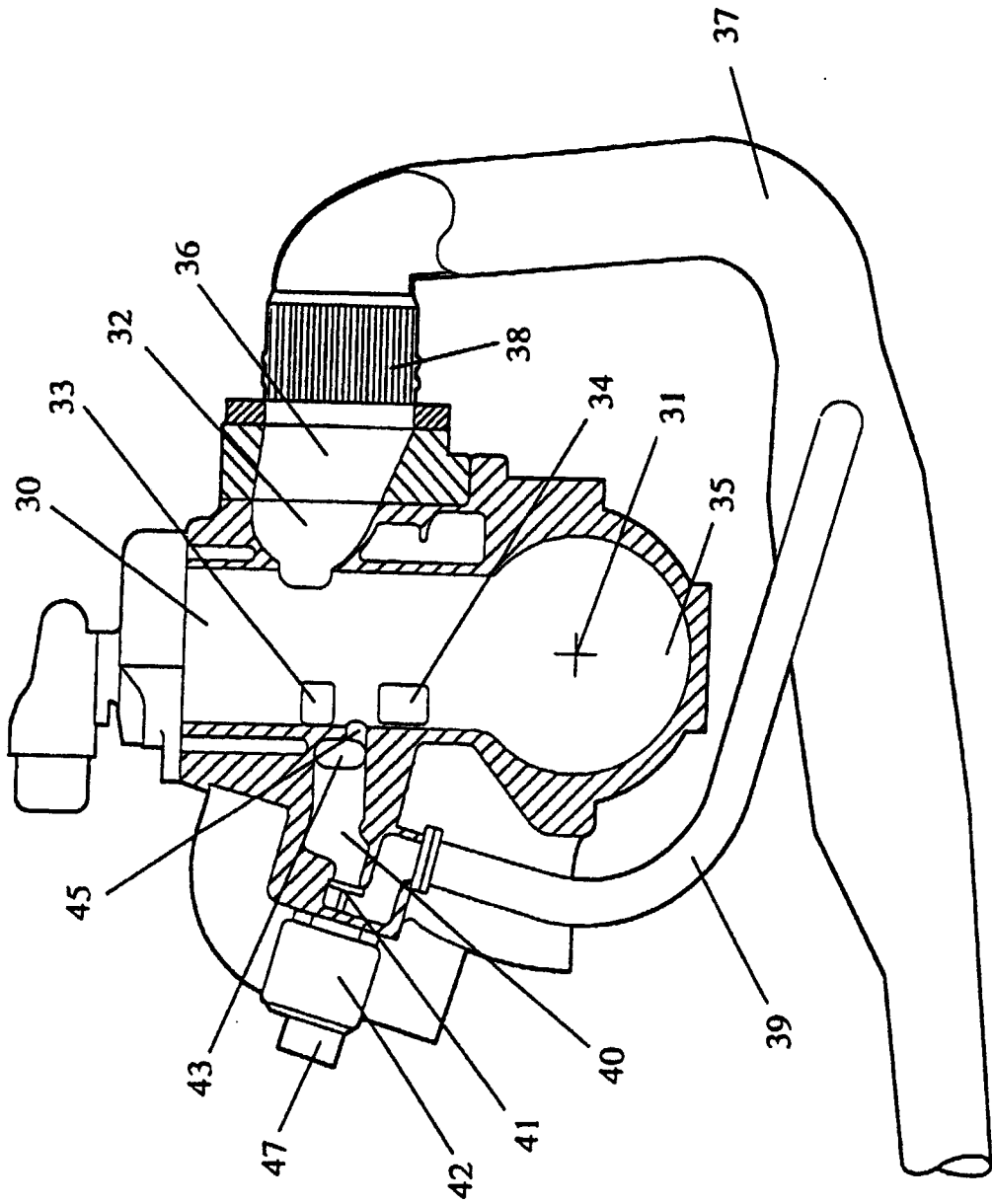


Fig. 1

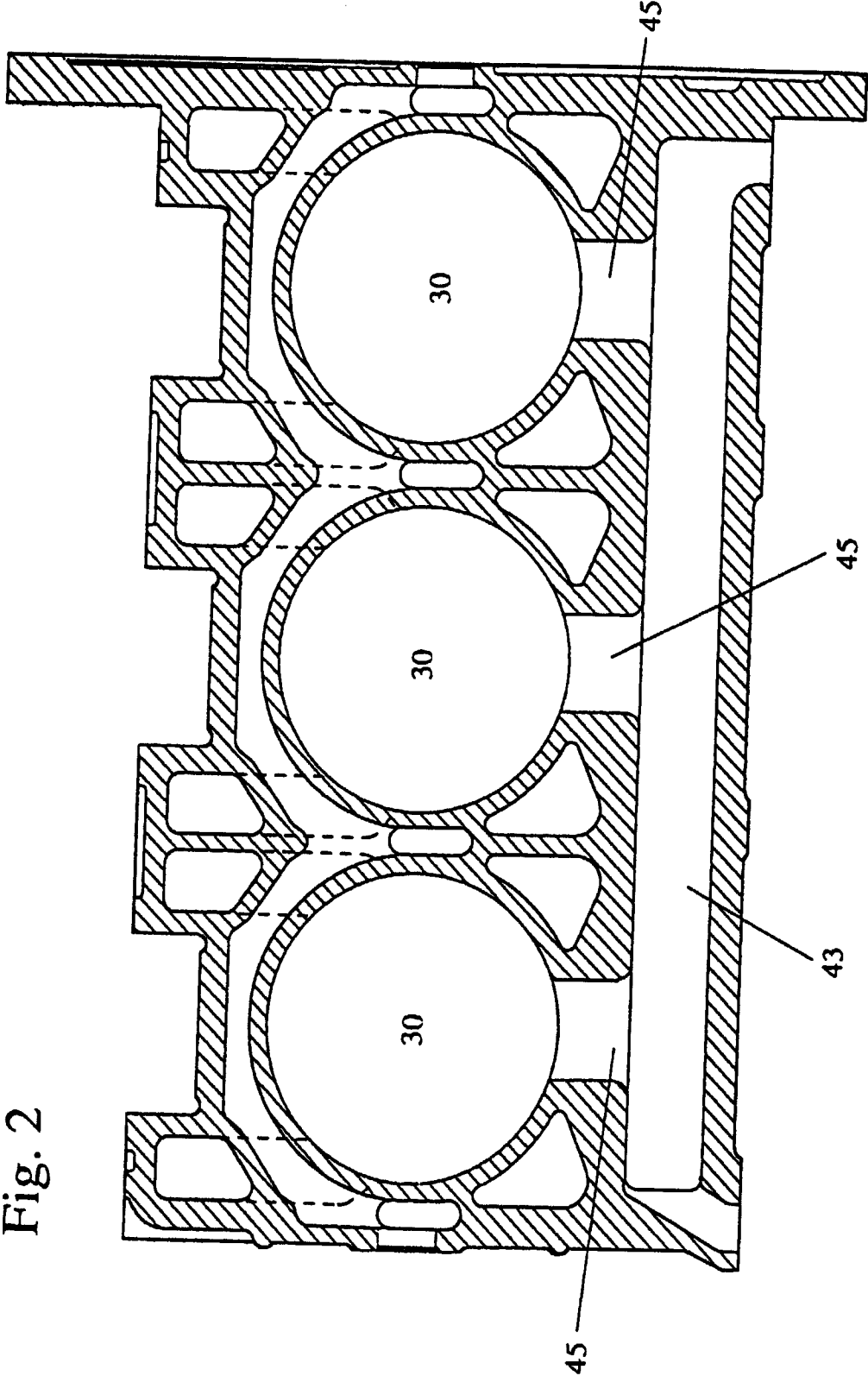


Fig. 2